

Tropical Cyclone Inner Core Dynamics

Assumptions

- Axisymmetric flow
- Gradient and hydrostatic balance above PBL
- Troposphere neutral to slantwise moist convection outside eye
- Moist adiabatic lapse rate in eye above inversion
- Well developed anticyclone at storm top

Local energy balance (from previous lecture):

$$\frac{M}{r_b^2} \cong - (T_b - T_o) \frac{ds^*}{dM}$$

Definitions:

$$\frac{f}{2} R^2 \equiv M = rV + \frac{f}{2} r^2 \quad \text{“potential radius”}$$

$$\chi^* \equiv (T_s - T_o) (s^* - s_a^*)$$

$$\chi \equiv (T_s - T_o) (s - s_a) \quad (s_a = s_a^*)$$

$$\chi_s \equiv (T_s - T_t) (s_{0a}^* - s_a) = \text{constant}$$

Scaling:

$$\chi^*, \chi \rightarrow \chi_s (\chi^*, \chi)$$

$$R, r \rightarrow \frac{\sqrt{\chi_s}}{f} (R, r)$$

$$\beta \equiv \frac{T_s - T_o}{T_s - T_t}$$

Scaled equations:

$$\frac{1}{r^2} = -\frac{2\beta}{R^3} \frac{\partial \chi^*}{\partial R},$$

$$R^2 = 2rV + r^2 \simeq 2rV \quad (\text{core})$$

$$\rightarrow \boxed{V^2 \simeq -\frac{R\beta}{2} \frac{\partial \chi^*}{\partial R}} \quad (1)$$

Conservation of angular momentum (dimensional):

$$\frac{dM}{dt} = -gr \frac{\partial \tau_{\theta}}{\partial p}$$

Integrate over depth of PBL:

$$\begin{aligned} \Delta p_b \frac{dM}{dt} &= -gr \tau_{\theta_s} \cong -gr \rho_s C_D V^2 \\ &\cong -gr \frac{p_s}{R_d T_s} C_D V^2 \end{aligned}$$

Scaling for time:

$$t \rightarrow C_D^{-1} \frac{R_d T_s}{g p_s} \Delta p_b \chi_s^{-1/2} t$$

Nondimensional angular momentum equation:

$$\frac{dR}{dt} = -r \frac{V^2}{R}$$

$$\text{But } r \simeq \frac{R^2}{2V}$$

$$\rightarrow \boxed{\frac{dR}{dt} \simeq -\frac{1}{2} RV} \quad (2)$$

Nondimensional PBL entropy equation:

$$\frac{d\chi}{dt} = \frac{C_k}{C_D} V (\chi_0^* - \chi) + \varepsilon V^3 - F_b, \quad (3)$$

$$\varepsilon \equiv \frac{T_s - T_t}{T_s}$$

Time derivative in R space:

$$\frac{d}{dt} = \frac{\partial}{\partial \tau} + \dot{R} \frac{\partial}{\partial R} + \omega \frac{\partial}{\partial P}$$

Assume χ well mixed in boundary layer,

use $\dot{R} = -\frac{1}{2}RV$:

$$\frac{\partial \chi}{\partial \tau} = \frac{1}{2}RV \frac{\partial \chi}{\partial R} + \frac{C_k}{C_D} V (\chi_0^* - \chi) + \varepsilon V^3$$

But $V^2 \simeq -\frac{R\beta}{2} \frac{\partial \chi^*}{\partial R} = -\frac{R\beta}{2} \frac{\partial \chi}{\partial R}$ *in eyewall*

$$\rightarrow \frac{\partial \chi}{\partial \tau} = \left[\frac{C_k}{C_D} V (\chi_0^* - \chi) - (1/\beta - \varepsilon) V^3 \right] \quad (4)$$

(Steady state solution:)

$$V^2 = \frac{1}{1/\beta - \varepsilon} \frac{C_k}{C_D} (\chi_0^* - \chi)$$

Differentiate (4) with respect to R and use $V^2 \simeq -\frac{R\beta}{2} \frac{\partial \chi}{\partial R}$:

$$\frac{\partial}{\partial \tau} \left(\frac{V}{\beta} \right) = \frac{1}{4} \frac{R}{V} \frac{\partial V}{\partial R} \left[3 \left(\frac{1}{\beta} - \varepsilon \right) V^2 - \frac{C_k}{C_D} \left(\chi_0^* - \chi \right) \right] \\ - \frac{1}{4} V^2 \left[2 \frac{C_k}{C_D} \frac{1}{\beta} + \frac{R}{\beta^2} \frac{\partial \beta}{\partial R} \right]$$

First two terms: Propagation; Second term: damping;

Third term: Possible amplification

From previously derived dependence of outflow temperature on angular momentum:

$$\frac{\partial \beta}{\partial R} = -\frac{1}{T_s - T_t} \frac{\partial T_o}{\partial R} = -\frac{Ri_c}{r_t^2} R^3 \frac{\beta}{2V^2}$$

Thus development equation becomes

$$\frac{\partial}{\partial \tau} \left(\frac{V}{\beta} \right) = \frac{1}{4} \frac{R}{V} \frac{\partial V}{\partial R} \left[3(1/\beta - \varepsilon)V^2 - \frac{C_k}{C_D} (\chi_0^* - \chi) \right] - \frac{1}{2} \frac{C_k}{C_D} \frac{1}{\beta} V^2 + \frac{1}{8} \frac{Ri_c}{r_t^2} R^4 \beta$$

Note that first term steepens V gradient when $V^2 > \frac{1}{3}V_{max}^2$

$$\frac{\partial \beta}{\partial R} < 0 \quad \textit{necessary for amplification}$$

V gradient cannot steepen indefinitely:

$$\zeta = \frac{V}{r} + \frac{\partial V}{\partial r},$$

$$\frac{\partial}{\partial r} = \frac{\partial R}{\partial r} \frac{\partial}{\partial R} = \frac{r}{R} \left(1 + \frac{V}{r} + \frac{\partial V}{\partial r} \right) \frac{\partial}{\partial R} = \frac{r}{R} (1 + \zeta) \frac{\partial}{\partial R}$$

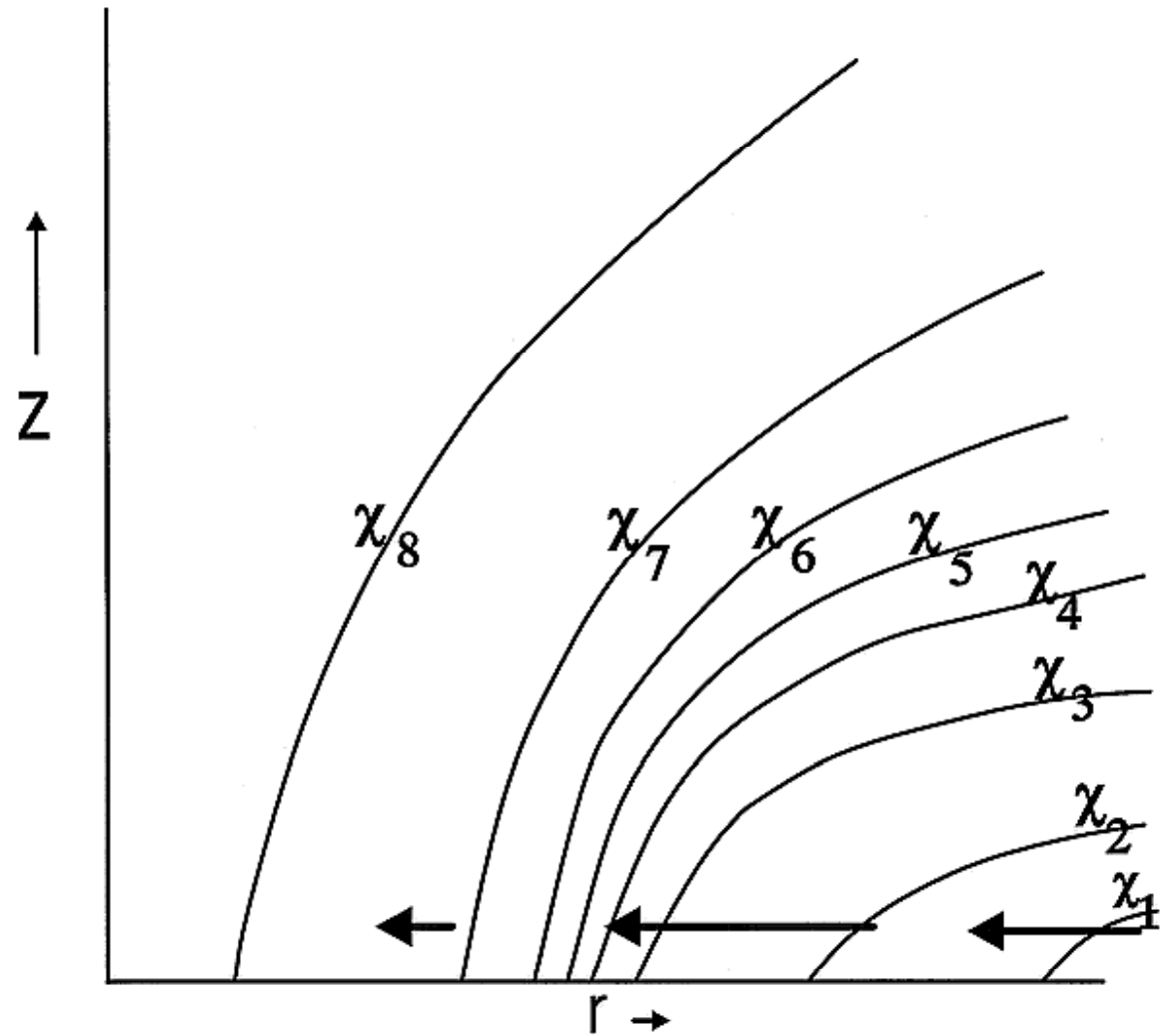
$$\rightarrow \zeta = \frac{V}{r} + \frac{r}{R} (1 + \zeta) \frac{\partial V}{\partial R}$$

$$\zeta = \frac{\frac{V}{r} + \frac{r}{R} \frac{\partial V}{\partial R}}{1 - \frac{r}{R} \frac{\partial V}{\partial R}}$$

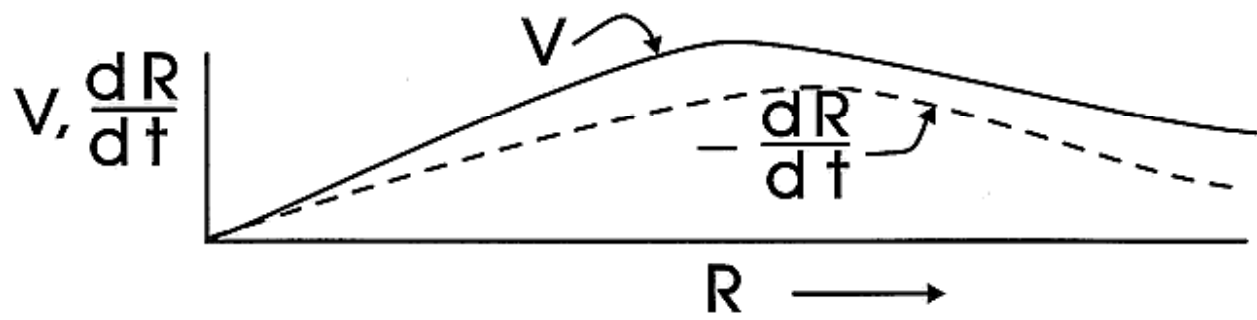
$$\zeta \rightarrow \infty \quad \text{when} \quad \frac{\partial V}{\partial R} \rightarrow \frac{R}{r} \cong \frac{2V}{R}$$

Eyewall undergoes frontal collapse!

This can only be prevented by 3-D eddies



$$\dot{R} \approx -\frac{1}{2}RV$$



Simplified amplification model:

$$\frac{\partial \chi}{\partial \tau} = \left[\frac{C_k}{C_D} V (\chi_0^* - \chi) - (1/\beta - \varepsilon) V^3 \right],$$

$$\chi_0^* = 1 - AP = 1 + A \left(\chi + \frac{1}{2} V^2 \right)$$

$$V^2 = -\frac{R\beta}{2} \frac{\partial \chi^*}{\partial R}$$

$$\frac{\partial \beta}{\partial R} = -\frac{1}{2} R^3 \beta \frac{Ri_c}{r_t^2} \frac{1}{V^2}$$

Enforce $\chi \leq \chi^*$

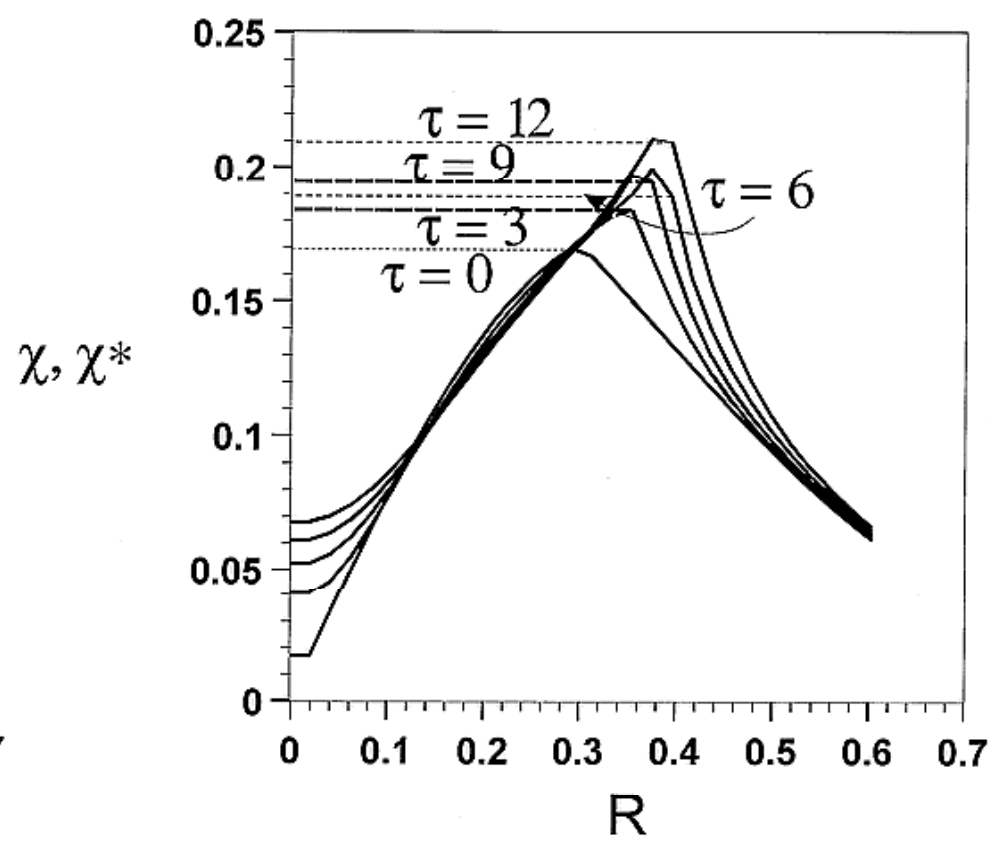
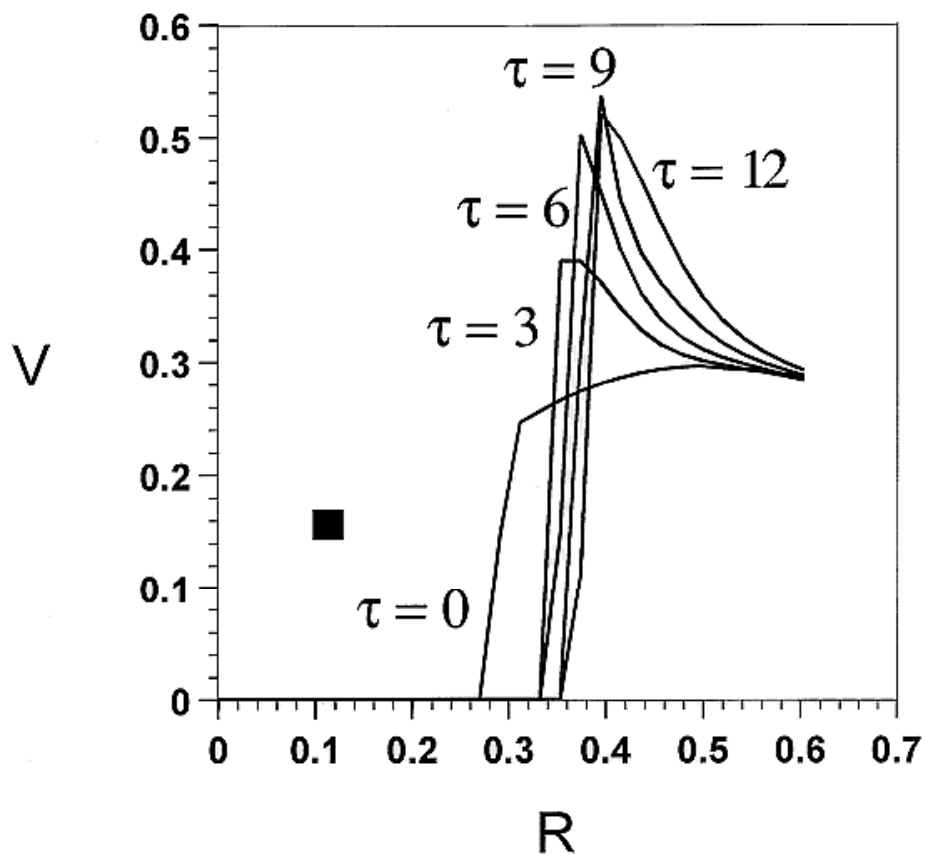
How to handle frontal collapse in model?

Three methods:

1: Zero diffusion model:

$$\begin{array}{l} \text{For } r < r_m: \\ V = 0 \\ \chi = \chi^* = \textit{constant} \end{array}$$

Does not prevent frontal collapse



2. Minimum diffusion model: Just enough radial diffusion to prevent failure of coordinate transformation.

From expression for vertical component of vorticity, we enforce

$$\frac{\partial V}{\partial R} \leq \frac{2V}{R}$$

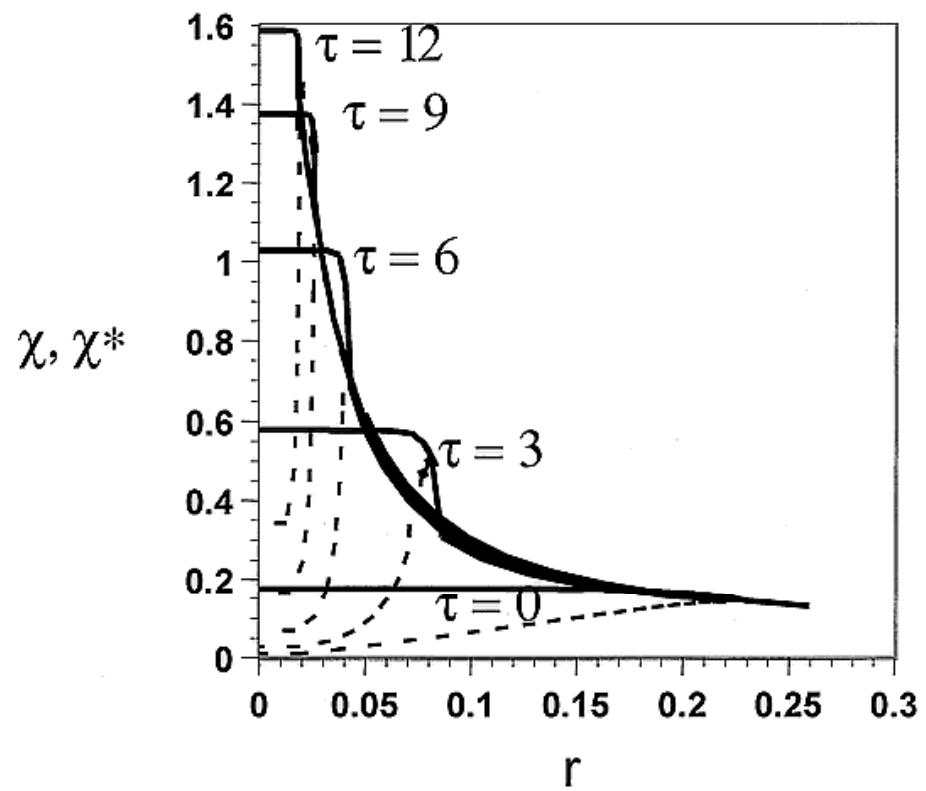
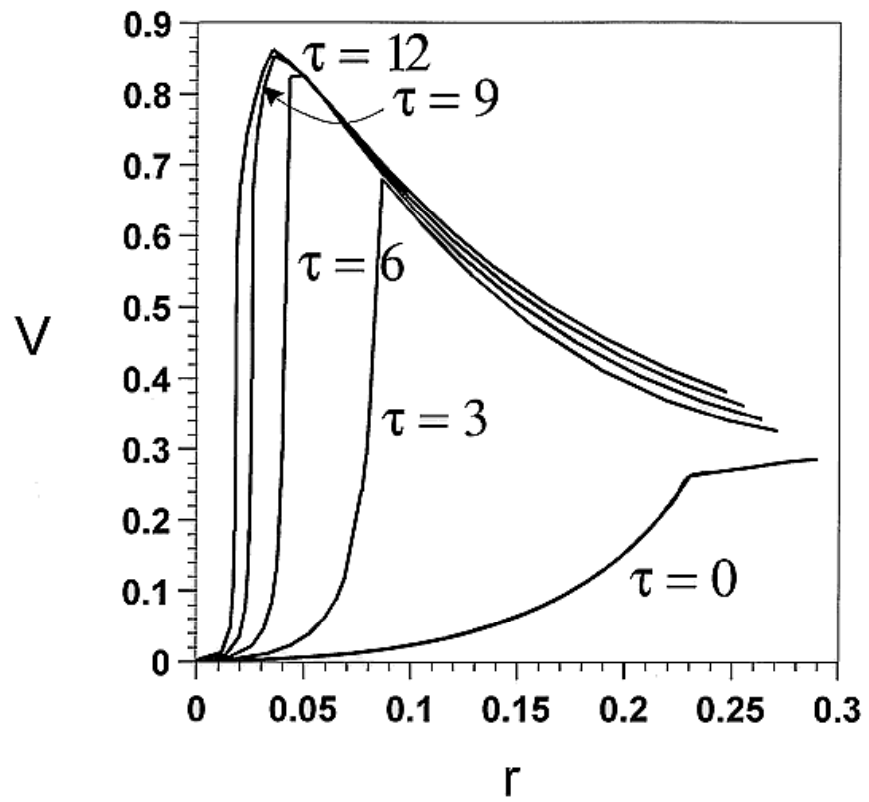
Inside the outermost radius, R_{crit} , where this is violated, we take

$$\frac{\partial V}{\partial R} = \frac{2V}{R}$$
$$\rightarrow V = V_{crit} \left(\frac{R}{R_{crit}} \right)^2$$

By integration of $\frac{\partial \chi^*}{\partial R} = -\frac{2V^2}{R}$

$$\chi^* = \chi_{crit} + \frac{1}{2} V_{crit}^2 \left(1 - \left(\frac{R}{R_{crit}} \right)^4 \right) \quad \text{for } R < R_{crit},$$

$$\chi^* = \chi \quad \text{for } R \geq R_{crit}$$

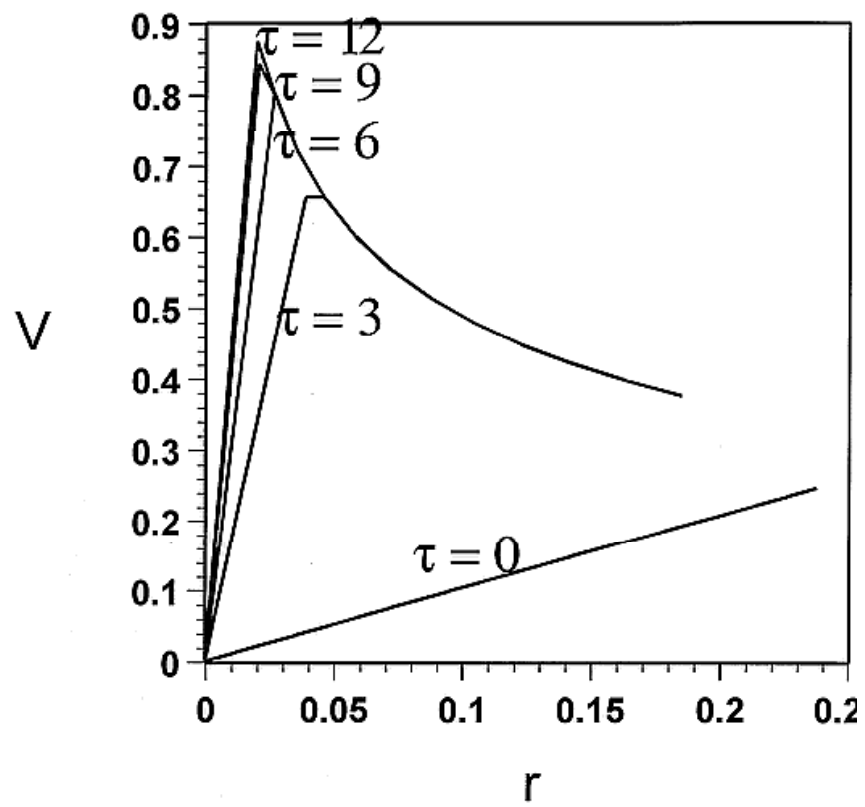


3. Maximum diffusion model: 3-D turbulence perfectly efficient in establishing constant angular velocity inside r_m :

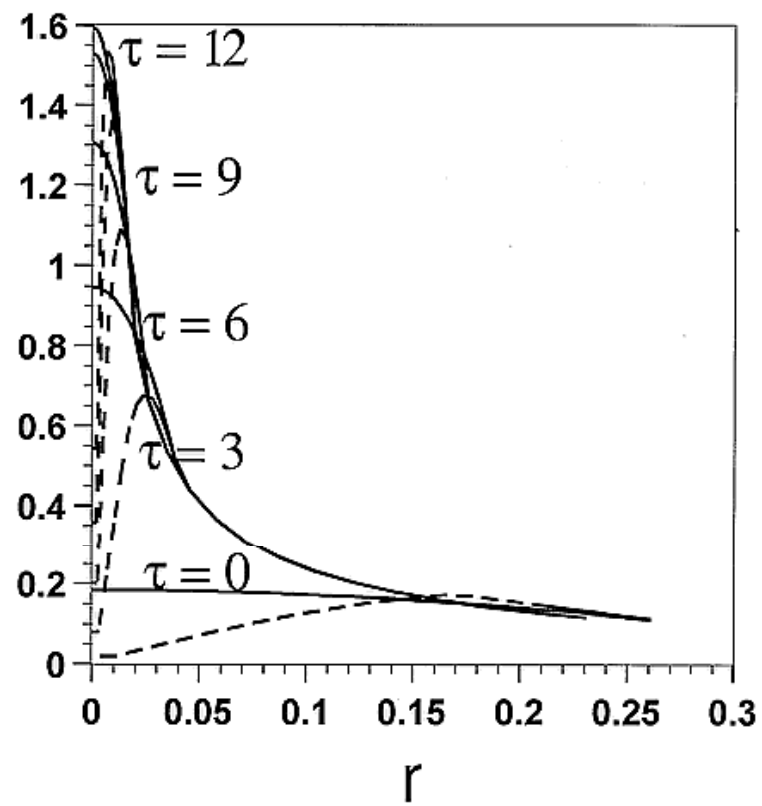
$$V = V_{max} \frac{r}{r_m} = V_{max} \frac{R}{R_m}$$

$$\chi^* = \chi_m + V_{max}^2 \left[1 - \left(\frac{R}{R_m} \right)^2 \right] \quad \text{for } R < R_m,$$

$$\chi^* = \chi \quad \text{for } R \geq R_m$$



χ, χ^*



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